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Interim Report

**AN ACCELERATED TESTING SYSTEM TO
DETERMINE PERCENT CRUSHED
AGGREGATE REQUIREMENTS IN
BITUMINOUS MIXTURES**

Thomas D. White
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PURDUE UNIVERSITY

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TO: Harold L. Michael, Director   June 11, 1990
       Joint Highway Research Project

                                                 Project: C-36-55J

FROM: Thomas D. White, Research Engineer
       Joint Highway Research Project   File: 2-12-10

    Attached is the Design Report on the HPR Part II study titled, "An
Accelerated Testing System to Determine Percent Crushed Aggregate Requirements
in Bituminous Mixtures." This design report is a product of Phase I of the
subject study. Subjects addressed in the study are procedures for estimating
accelerated structural and rutting damage, refined design and cost estimate
and proposed experimental design to determine the minimum crushed aggregate
requirements in bituminous mixtures.

    Estimates of the time of testing to develop structural and rutting damage
have been made. In both cases the projected cycles of loading are within the
initial criteria of equaling the damage in 10 years of interstate type traffic
with one year of continuous operation. Design of the Accelerated Testing Sys-
tem (ATS) was constrained to achieve the initial criteria. In fact, the
analysis suggests that the ATS, as designed, will easily achieve the stated
goal. Detailed material and labor costs by subsystem as well as by specific
item are presented based on the proposed design. An experimental design has
been developed with input from INDOT, Purdue and aggregate industry represen-
tatives.

    This report is forwarded to INDOT and FHWA in fulfillment of the Phase I
objectives of the study.

                            Respectively submitted,

                            T. D. White
                            Research Engineer

TDW/rrp

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AN ACCELERATED TESTING SYSTEM TO
DETERMINING PERCENT CRUSHED AGGREGATE REQUIREMENTS IN
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and

John E. Haddock, Sr.

Joint Highway Research Project

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16. Abstract

With increase in axle loads, tire pressures and volume of truck traffic there has been an increase in the rate of which bituminous pavements are exhibiting rutting. Because resistance to rutting can be increased by the addition of crushed aggregate, a need exists for a method of determining what amount of crushed material is required and the characteristics of that crushed material to optimize performance and economy.

The Accelerated Testing Facility will be located at the INDOT Research Division Facilities in West Lafayette, Indiana. A pit within the Test Facility will allow prototype scale pavement sections to be installed. An Accelerated Testing System has been designed that will span the pit and incorporate the capability to apply moving wheel loads. Materials used in the test sections as well as environment and loading conditions will be controlled. Structural damage will be scaled by increasing the load so that greater pavement damage is incurred by each pass of the load. Rutting distress will be scaled by increasing asphalt mixture temperature and thereby decreasing the mixture stiffness. Reduced stiffness would increase rutting distress with each load that passes.

A number of pavement materials, structure and loading factors can be evaluated in the facility. Subsequent phases of the study will address the relative performance of asphalt mixtures prepared with varying amounts crushed aggregate.

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Introduction

With increase in axle loads, tire pressures and volume of truck traffic there has been an increase in the rate of which bituminous pavements are exhibiting rutting. The resistance to rutting of conventional bituminous mixture depends on a number of factors related to its constituents. One important constituent is the nature and the amount of crushed aggregate. However, it is important to consider economy and the use of local materials. Local materials may mean sand and gravels which are available in many parts of Indiana. Economy may come from the lower cost or shorter hauling distance. The desire for economy and use of local materials is offset by the need to insure that bituminous mixtures used in surfacing the highway pavements in Indiana will provide the desired performance. Because resistance to rutting can be increased by the addition of crushed aggregate, a need exists for a method of determining what amount of crushed material is required and the characteristics of that crushed material to optimize performance and economy.

Tests on small, laboratory size specimens do not reliably scale to performance of prototype pavements. Prototype pavement test sections can solve the problem of scale, however, differences in performance may take many years to develop. An alternative testing procedure is to consider testing a small section of pavement with prototype loads. Such testing may utilize techniques

to reduce the time for performance differences to develop. Structural damage may be scaled by increasing the load so that greater pavement damage is incurred by each pass of the load. Rutting distress may be scaled by increasing asphalt mixture temperature and thereby decreasing the mixture stiffness. Reduced stiffness would increase rutting distress with each load that passes.

A "Traffic Simulator" or accelerated testing system (ATS) has been designed with which simulated truck traffic can be applied to a small section of pavement. Materials used in the test sections as well as environment and loading conditions can be controlled. A number of pavement materials, structure and loading factors can be evaluated in the facility. The current study will address the relative performance of asphalt mixtures prepared with varying amounts crushed aggregate.

Other types of paving materials such as modifiers can also be evaluated with the ATS. Laboratory results indicate that such materials increase bituminous mixture high temperature stability without reducing their performance at low temperatures. In fact, in some cases there is a potential for these materials to provide even better low temperature properties while maintaining high temperature stability. By selecting the proper scale of the ATS and developing an adequate design, structural capacity of pavement systems can also be evaluated.

The Accelerated Testing Facility will be located at the INDOT Research Division Facilities in West Lafayette, Indiana. A pit within the Test Facility will allow prototype scale pavement sections to be installed. The ATS will span the pit and incorporate the capability to apply moving wheel loads. Design and characteristics of the ATS and its application to the study of

pavement structural and material factors are discussed in the following sec-
tions. Plans are also presented for the study of the minimum crushed aggre-
gate requirements in bituminous mixtures.

Literature Review

Traffic Simulators

Over the years, a number of different designs of "traffic simulators"
have been used in pavement research. Use of a traffic simulator is the direct
result of the researchers´ need for more timely and accurate data. The simu-
lators allow for data to be obtained under controlled conditions. At the same
time the data is more realistic. Types of simulators can be grouped according
to size (i.e. large, medium, and small).

Large Simulators

The large simulator class generally includes simulators which are out-
doors and if indoors, require more than an average size laboratory for their
operation. These simulators range all the way from the test tracks at the
United States Army Corps of Engineers Waterways Experiment Station to the cir-
cular test track at Washington State University.

One of the earliest applications of simulated traffic under controlled
conditions in pavement research was conducted by the US Army Corps of
Engineers (USAE) at the Waterways Experiment Station (WES). In traffic tests
that developed the original Marshall bituminous mix design criteria (Depart-
ment of the Army Technical Memorandum No. 3-254, 1948), wheel loads of 15,000;
37,000 and 60,000 lbs with tire and contact pressures shown below were used to
apply accelerated traffic in amounts up to 3,500 coverages. A coverage is

defined as the number of passes to cover the full width of a test lane with a given width tire. In the final analysis, much of the comparison of the mixture properties was made at 500 and 1,500 coverages of the applied traffic.

Gross Loads-Lb	Load per Tire-Lb	Inflation Pressure-PSI	Gross Contact Pressure-PSI	Net Contact Pressure-PSI
15,000	15,000	50	54.3	105.6
37,000	37,000	110	98.7	146.2
60,000	30,000	110	91.3	139.2

Earlier laboratory tests included samples with asphalt contents that bracketed the optimum asphalt content as determined by the peak of the stability curve. Subsequent experience with test sections at Marietta, GA indicated that optimum selected at the peak of the stability curve would be overrich. Consequently, the test sections at WES were constructed at optimum and 10 and 20 percent lean of optimum. The traffic tests were planned and conducted not only to compare paving mixtures with variable properties and identify traffic related optimum asphalt content ranges, but also to determine minimum thickness of asphalt surfacing over low and medium quality bases.

In tests of base courses conducted by Maxwell, et al. (1962), three different vehicle load carts were used. The three vehicles were configured and loaded to apply a 10,000 25,000 and 50,000 lb. single-wheel load, respectively.

The 10,000 lb. vehicle consisted of a loaded axle powered by the front half of a four wheel drive truck. A type I 34:00-9.9, aircraft tire was used inflated to 100 psi. The 25,000 and 50,000 lb. load carts were pulled by a

tractor on which were mounted a 56:00-16, type I, and a 25:00-28, type III,
aircraft tire, respectively. Both tires were inflated to 100 psi.

In these tests, the pavement test sections were constructed in an open
ended aircraft hanger and therefore were isolated from rainfall. The test
sections were 12 feet wide by 150 feet long. Traffic was applied on three
four feet wide lanes. These lanes were trafficked such that each lane was
loaded with specific loads a specified number of times. The purpose of the
test was to evaluate base courses using various loads and tire pressures. The
base course itself consisted of a graded crushed limestone. After compaction
and prior to traffic, a bituminous seal coat was applied.

The two primary conclusions of the above study were: (1) Occasional
traffic overloads applied to pavement does in fact shorten the life of the
pavement even if the load does not cause immediate and drastic damage; and (2)
the number of passes of basic traffic needed to equal one pass of an overload
varys directly with the thickness and condition of the pavement and base
course.

A similar test was conducted at WES and reported by Ledbetter, et al.
(1972) to determine the effects of "jumbo jets" on pavement performance. Five
test sections for this experiment were built in an area 60 feet wide and 300
feet long. Each pavement section was trafficked in a previously specified
manner. Four different test vehicles were used. One of the vehicles used was
a cart configured to represent one-half the main gear of a C5A military tran-
sport aircraft. This twelve wheel assembly was loaded so that each wheel car-
ried a 30,000 lb. load. The tires were inflated to 100 psi. A second cart
was configured to represent the twin-tandem gear of the Boeing 747. In this

test, the cart was loaded at 60,000 lb. per wheel (1,000,000 lb. loading con-
dition for the entire aircraft - an overload condition). The tires were
inflated to a pressure of 225 psi. Two other carts were configured for a
30,000 lb. and a 50,000 lb. single-wheel load, respectively. The former had a
tire pressure of 100 psi, and the latter a pressure of 165 psi.

The major conclusions reached in this report were that the higher repeti-
tions of these heavy, many-wheeled vehicles was more favorable than previous
theory had indicated, and the measured stress and deflection are not well
predicted by sophisticated linear theoretical treatments (Ledbetter, et al.,
1972).

A test track used by Paterson (1972) consisted of an octagonal annulus
located outdoors at the University of Canterbury in Christchurch, New Zealand.
The track had a mean diameter of 60 feet and the actual track was four feet
wide. Traffic was applied with two sets of dual tires at either end of an arm
extending across the diameter of the track. The center pivot was eccentri-
cally located so that the wheels tracked a path which included wander. Con-
crete ballast was used for loads ranging from 3000 lbs. to 9000 lbs. The
apparatus was capable of maintaining a constant speed of 12 mph. Power was
supplied by an electric motor on one set of wheels and the other wheels were
free turning. The tires used were 9.00 x 20 x 12 ply.

For a study of transient and permanent deformations in asphaltic concrete
pavements, Paterson used bituminous mixture placed on 11 inch thick concrete
slabs. Within these slabs, heating elements were placed to keep the pavement
within 2 degrees of the desired temperature. As a result, the response of
bituminous mixtures at different temperatures and loads could be studied.

Use of a circular test track at Washington State University was reported by Kingham and Kallas (1972), and Mahoney and Terrel (1982). This traffic simulator has three sets of dual wheels each connected to the center by a radial arm. Load is applied through weight of the structure as well as a water tank. Each of the inside wheels is driven by an electric motor while the three outside wheels turn freely. An eccentric mechanism allows for wander. The test track diameter is 84 feet and the wander is spread over a 4 feet width.

Kingham and Kallas (1972) compared three pavement bases, a bituminous concrete base, a sand bituminous base, and a crushed stone base. The purpose of the study was to relatively evaluate base performance under simulated in-service conditions, as well as to see if laboratory tests could predict in situ pavement performance. Their conclusion was that the laboratory experiments did predict fairly well the actual performance of the pavement under the action of the traffic simulator.

Mahoney and Terrel used the Washington State simulator to study the performance of three bituminous mixtures. One mixture was dense graded and the other two contained a sulfur additive. These results were also compared with laboratory tests.

In 1977, Sharma, et al. reported on work at the Pennsylvania State University Test Track to correlate actual pavement performance and response with that predicted by the FHWA program VESYS IIM. The Penn State Test Track is a one mile oval. One end of the oval has a -1% grade and a design speed of 50 mph. The other smaller end of the oval has a +1% grade and a design speed of 35 mph. Tangent sections are on 0.3% grades and are constructed so that

one is totally in cut and the other totally in fill. Traffic was applied by a standard truck tractor pulling trailers loaded with ballast (metal ingots). By changing the size, amount, and location of the ballast, the axle loads could be varied. The study concluded that the program did indeed give reasonable results. However, it was felt that local data would be needed for calibration to local conditions.

In Switzerland, Scazziga (1982) used a traffic simulator to re-evaluate the design procedures for flexible pavements. The simulator has three radial arms each having dual truck tires (11.00-20) loaded to 5 tons. The tires track around a ring having an average radius of 16 meters. Each wheel assembly is powered by an electric motor. The pavement structure was constructed in a concrete pit two meters deep. Scazziga concluded that the AASHTO Interim Guide Method (1972) provided for the thickest and most conservative designs.

A large circular traffic simulator is also located at the Laboratoire Central des Ponts et Chaussees (Public Works Research Laboratory) in Nantes. This track has an outside diameter of 41 meters and is 6 meters wide. Four arms, each 14 meters long, rotate around the circular facility. At the end of each arm is a half axle which can slide in and out on the arm to allow for trafficking at different radii as well as providing for wander. The unit is driven by four slow-speed hydraulic motors situated at the center turret. Research was conducted with the simulator to determine if test results would be realistic. It was the conclusion of the researchers that the traffic simulator provided realistic data (Autret, et al., 1987).

Medium Simulators

Although most medium size simulators are outside where the test pavements

are exposed to the elements, the simulators themselves as well as the test sections are smaller than those in the large group.

In 1967, Gusfeldt and Dempwolff reported on the use of a traffic simulator for pavement research in Germany. The simulator consisted of two parallel steel girders which supported a dolly between them. A test wheel was mounted on the dolly. The wheel had a diameter of 100 cm and was usually inflated to a pressure of 5 kp/cm^2. An electric motor powered the load wheel via a drive cable and could attain a top speed of 50 km/h. Load was provided by means of a pneumatic system which used the two girders as reaction beams. The system was capable of providing a load of between 0.4 and 2.0 tons. Test sections to which traffic was applied measured 10 x 10 meters with 30 meters on either end to provide for the acceleration and deceleration of the dolly. The traffic simulator described can easily be disassembled to allow normal construction techniques to be used for test sections.

Pavement stresses and strains were determined using the traffic simulator. It was concluded that the results obtained were in good agreement with the results predicted by theory. This agreement warranted further testing using the simulator.

In additional work, Dempwolff and Sommer (1972) measured radial strains (longitudinal and transverse) and vertical strains in a bituminous layer along with vertical stresses in the unbound base and soil layers. Using a single-wheel (9 x 20 x 10 ply) inflated to a pressure of 5 bars, results were obtained on the effects of temperature, loading time, bitumen grade, and bituminous mix properties.

Research by Brown and Pappin (1982) made use of a "Pavement Test Facil-
ity." This simulator was configured with one wheel with a diameter of 560 mm
which could be loaded up to 15 kN. Load was applied by means of a hydraulic
ram which reacts against a steel girder spanning the test section parallel to
the direction of wheel travel. The trafficked test section was 4.8 meters
long, 2.4 meters wide, and 1.5 meters deep. In their work, the simulator was
used to continue the development of analytical procedures for predicting pave-
ment performance. They concluded that the simulator was a valuable tool in
validating analytical design methods.

The "Heavy Vehicle Simulator" (HVS) used in South Africa is described by
van Vuuren (1972). Mounted on a wheeled frame, the HVS can be transported
under its own power to conduct in situ pavement traffic tests. Once at a test
site, the trafficking wheel is mounted for testing. The load may be applied
to tires ranging in size from a 5.20 x 10 to a 14.00 x 20. Load is applied by
hydraulically reacting against the frame and can range from 20 to 80 kN. A
hydraulic motor with a chain drive provides power. Traffic an be applied in
both directions at a speed of 10 km/h. The tire can track in an area 6 meters
long and 1 meter wide. Lateral wander of the tire is allowed for with the
system.

A number of South African researchers have used the HVS. Freeme, et al.
(1982) reported on the use of the HVS in the development of a mechanistic
pavement design procedure in South Africa. Viljoen, et al. (1987) used the
HVS to test the resistance to crackings of conventional and innovative over-
lays.

Additionally, use of the HVS was reported by Hugo, et al. (undated) for

research aimed at investigating the influence of low temperature and aging on premature cracking. For this study, special equipment was added to the HVS. The special equipment allowed for cooling as well as accelerating pavement aging. A cooling chamber was constructed around the load tire large enough to cool 2.5 meters of the 6 meter test section. Aging was stimulated by using infra-red and black lights in sequence. A 2 x 2 meter section of the test pavement could be aged.

The conclusions of this study were that low temperatures do initiate early cracking in pavements and that cracking in aged pavements is a complex phenomena.

Ferreira, et al. (1987) used the HVS in investigations into the performance of recycled materials in pavements. In this study, test pavements consisted of two 50 mm base layers each containing 70% reclaimed material and a new 40 mm wearing course. Applied loads ranged from 70 to 100 kN. The researchers concluded that the behavior of recycled material was a function of the support provided by the subbase layers. If support was adequate, the recycled material performed according to design. It was further determined that if cracking did occur, the pavement life could be extended by preventing water infiltration.

As an alternative to the HVS, researchers in Australia developed the "Accelerated Loading Facility" (ALF). The specifics of this simulator were presented by Kadar (1987) in a study designed to set up and test pavement monitoring systems. This study was also used to design a system for containing monitoring pavement structural performance. Both of these goals were fulfilled by using ALF. The ALF simulator makes use of a steel support frame.

Ballast is used to provide load which may be varied from 4 to 8 tons in 1 ton increments. The wheel assembly is accelerated to a speed of 20 km/h by rolling down a ramp and across a 12 meter test section. Deceleration occurs when the tires run up a second ramp. The tires return to the starting point by rolling along a steel plate located on the underside of the upper support beam. This allows the wheels to continue rotating in the same direction at all times. Wander is provided for by moving the entire frame transversely. By addition of wheels attached to the frame, ALF becomes mobile so that in situ pavement can be trafficked.

The Federal Highway Administration (FHWA) has purchased the design and built an ALF system which is currently in operation at the FHWA Turner-Fairbanks Research Laboratory in McLean, Virginia. A number of interesting studies are currently underway using this equipment.

Small Simulators

Small traffic simulators are for the most part installed in laboratories. They are viewed as a laboratory tool which can simulate some of the effects of traffic. They are not, generally speaking, as effective as the larger simulators that have previously been described. One limitation of the small traffic simulators is that the pavements tested cannot be placed by normal construction methods. Results of trafficking tests are therefore limited.

One of the small laboratory simulators that has been used effectively is the "Rolling Wheel Machine," or as it is sometimes called, the "Road Test Machine" built and used by the Royal Dutch/Shell Group. This simulator has a 3 meter circular track where the test sections are constructed between two concrete walls. A beam with a wheel at either end is attached to a center

pivot. The wheels rotate around the pivot. Speed can be varied over a range up to 18-20 km/h. Loads between 100 and 2000 kg are applied hydraulically.

Bazin and Saunier (1967) reported on use of the Royal Dutch/Shell simulator in research studying the properties of bituminous materials. Klomp and Niesman (1967) presented work using the same simulator to examine strains in flexible pavement at different speeds. They conclude from their tests that the tensile strain was reduced 40% when speed was increased from 1 km/h to 16 km/h.

Hofstra and Valkering (1972) and Hofstra and Klomp (1972) also conducted research with the Royal Dutch/Shell simulator. The first research was done to determine if elastic theory represented the behavior of flexible pavement under the action of moving wheels. Their findings were that the elastic theory did agree well with the data obtained in the laboratory. The second study was designed to examine pavement rutting. Temperature effects on rutting was part of the study. Data showed that rutting over a temperature range of 20-60°C was much greater than the increase in rutting predicted by elastic theory. Both of these research efforts required that the simulator apparatus include some facility for heating the pavement. Heating was accomplished by the addition of thermal hoods which were mounted on the beam. The thermal hoods rotate with but are slightly ahead of each of the wheels.

A simulator was built at the University of Illinois Urbana-Champaign (UI) in conjuction with testing on several sections continuing pozzolanic materials. Barenberg (1967) describes the simulator. The UI simulator is described as a "Loading Frame" weighing 3500 lbs. With ballast the total weight could be increased to 6400 lbs. This frame rotated about a center pivot. A wheel

was attached to either end. Top rotation speed was 25 rpm. Wander was included in the test by means of small oscillations of the simulator.

Eisnmann and Hilmer presented a paper describing the use of a "Test Facility" to study the influence of wheel loading and inflation pressure on rutting of pavements in Germany. The facility used was a tire pair configured as either two separate tires or one set of dual tires. Materials to be tested were placed in a steel box. A rubber mat of known elastic properties was used to simulated the foundation support. The rolling speed of the wheels was 1 km/h with a loading frequency of about 2.5 seconds. This slower speed caused faster rutting of the material than would normally occur. The report concluded that wheel load, inflation pressure, average contact pressure, and tire arrangement have an important effect on rutting.

Accelerated Rutting Due to Decreased Mixture Stiffness

In order to study rutting and the minimum crushed aggregate requirements, test pavement rutting will be accelerated. One way this can be accomplished is by increasing the bituminous mixture temperature and thereby decreasing its stiffness. Since bituminous material is a viscoelastic material, the theory behind this method is simplified.

Papazian (1962) presented work on the response of viscoelastic material in the frequency domain. Two pertinent conclusions were reached in the study. First, the asphalt concrete shows a higher degree of elasticity with a higher rate of loading. In fact, Papazian concludes that at a very high loading frequency, the real part of the elastic modulus approaches a value of instantaneous elasticity. Secondly, the permanent deformation is both a function of number of load applications and duration of loading. The longer the duration

or the greater the number of loads, the greater will be the permanent deformation.

Hofstra and Klomp (1972) in their work with the Royal Dutch/Shell simulator indicate that with an increasing number of repetitions, the permanent deformation per pass decreases. Their study also included studies on the effects of temperature on deformation. Deformations are related to the binder viscosity. Therefore, the viscosity is merely another measure of the stiffness of the mix. A stiffer material is more viscous.

Minimum Crushed Aggregate Content

One aspect of bituminous mixtures which will be addressed in this study is the minimum crushed aggregate content. Since crushed aggregate is more expensive than pit run aggregate, money can be saved by using as much pit run material as is feasibly. This, however, can create problems if not enough crushed material is used. One problem which can arise in this situation is rutting.

Several research efforts have been directed toward crushed aggregate requirements in asphalt mixtures. One example is a study done in 1987 by Regan at the USAE Waterways Experiment Station. His research examined the role of high pressure (350-400 psi) aircraft tires in rutting. Crushed limestone aggregate blends were used in combination with three different binders. Asphalt paving grades of AC 20, AC 40, and a modified AC 20 were used in Marshall specimens prepared using 75 blows per face with a manual handhammer. Additional samples were prepared using a gyratory compactor. Laboratory tests conducted in the study included indirect tensile (static and dynamic), direct shear tests, accelerated aging tests, and unconfined creep tests. The study

found that current heavy-duty design methods were adequate. However, it was concluded that more compaction was needed to avoid rutting and densification.

A laboratory study conducted by Akhter and Witczak (1985) compared mixes of crushed stone, gravel, slag, and sand. Using the amassed data, a simulation was done on pavement models for fatigue and rutting. A regression equation was developed to predict these performance characteristics.

In 1985, Hicks, et al. reported on a study for the Alaska Transportation Department to determine an approach for using crushed aggregate in airfield and highway pavements. They used laboratory analysis to determine the effects of fracture and gradation on both aggregate bases and asphalt concrete.

Eppensteiner, et al. (1979) conducted a study to relate laboratory tests on bituminous pavements to actual performance. The experiment involved constructing 44 test sections using 20 different aggregates and then observing the pavements performance over a five year period. An attempt was made to develop a numerical relationship between laboratory performance and in situ performance but was unsuccessful.

In a report by Kraemer in 1966, recommendations were made that 70% crushed stone and 30% rounded-stone are preferable for bituminous mixtures because maximum compaction could be obtained which corresponded to maximum stability.

Accelerated Damage Due to Load

Pavement damage can be accelerated by increasing loads. For example, the effect of increasing an 18 kip axle load (9 kips per half-axle) can be estimated using the AASHTO load equivalency factors (Yoder & Witczak, pp.

147-150). With increased load the damage per pass is multiplied. As a result, the time to achieve a total amount of damage can be reduced.

The AASHTO load equivalences factors (LER) were derived to relate the loss in serviceability of the pavement caused by a given vehicle to the loss in serviceability caused by a standard vehicle (18 kip axle). Using the AASHTO LEFs (ibid pp. 164-167) and given the number of load repetitions of the standard vehicle to cause a terminal serviceability, the number of repetitions of the given vehicle to reach the terminal serviceability can be determined. Using the AASHTO LEFs a set of relations can be developed for the number of load repetitions of the half-axle load of the ATS to reach a terminal servi-ceability. To determine the required load needed on the ATS, the number of repetitions of the standard load to failure can be equated to the number of load repetitions of the ATS which can be applied in the given time frame. These two values then fix the load which must be applied by the ATS to obtain an equivalent loss in serviceability.

Based on calculations using reasonable structural capacity (10 inch rigid slab and SN=6 (CBR=3) for flexible pavement), P_t=2.0 and assuming ten years of highway traffic to be 35 million 18 kip equivalent axle loads, curves have been prepared for both rigid and flexible pavements. Using these curves, the load which must be applied by the ATS can be determined.

Since many different loads and number of load repetitions can be pro-jected the real limiting factor becomes time. How much time should be spent trafficking the pavement? At the outset of the project it was stated that the desirable and realistic goal was to compress 10 years of highway traffic into 1 year or less of simulated traffic. The limiting time period therefore

becomes 1 year. Assuming that there are approximately 200 working days in the year and that the ATS will have down time for repair, cleaning and maintenance, a reasonable assumption can be made of 120 days of operation per year (60% of 200 days).

To evaluate speed and load effect a matrix involving different loads, speeds, and time is shown in Table 1. As may be seen for each of the loads there is a significant reduction in the time requirements if the ATS speed is increased from 3 to 7 mph. Furthermore, the time for the projected number of load repetitions is substantially reduced if the ATS load is increased from 15 to 20 kips.

Values in Table 1 were calculated using reasonable assumptions. The distance the wheel would travel was assumed to be 22 feet. A width of 20 feet is planned for the test pit and an additional foot was added at each end for extra distance to stop, reverse, and restart the wheel. It was further assumed that the time needed to stop, reverse, and restart the wheel is negligible. This assumption seems valid in light of the fact that the speeds involved are all below 10 mph and that the simulator is loaded by springs rather than ballast.

Estimate of Rutting Damage

In addition to traffic, speed and temperature are two major factors expected to contribute to compression of time of testing for rutting damage to develop. A reduction of speed would increase the loading time and the viscous component of deformation. An increase in temperature would have the same effect. The magnitude of the speed and temperature effect can be estimated using the Shell method (Classen, et al., 1977).

		SPEED (MPH)	HOURS	DAYS
	15	3	4,861	203
		5	2,917	122
		7	2,083	87
	17.5	3	2,778	116
		5	1,667	69
		7	1,190	50
	20	3	1,528	64
		5	917	38
		7	655	27

SIMULATOR LOAD (KIPS) (row label spanning the left column)

TABLE 1. Time needed to compress ten years of traffic into one year of continous simulator operation.

Temperature, loading time and traffic are accounted for in the relation:

$$S_{bit,visc} = \frac{3}{t_w \Sigma(\frac{N}{\eta})_T}$$

$S_{bit,visc}$ = Viscous component of bitumen stiffness

t_w = Time of one wheel pass

N = Number of wheel passes

η = Viscosity

T = Test temperature.

In the denominator of the right hand side of the equation, the term $\Sigma(\frac{N}{\eta})_T$ represents the summation of traffic effects applied at different times of the day, throughout a year. Such a summation accounts for daily and yearly temperature variations. The Shell method uses six daily periods and twelve annual periods. The summation of traffic and temperature interaction results in an effective viscosity such that:

$$S_{bit,visc} = \frac{3\eta_{eff}}{t_w N}$$

For purposes of estimating the $S_{bit,visc}$ for Indiana, η_{eff} values associated with Chicago for a hardened 50 pen asphalt and a hardened 100 pen asphalt were selected from the Shell Pavement Design Manual (1978). Time of loading

is based on mean highway speed in Indiana (Coree and White 1988) and is taken
as the time for a truck to travel the diametric distance of circular loaded
area determined for a 4500 lb load and 100 psi tire pressure. The resulting
values of $S_{bit,visc}$ are:

		Hardened 50 pen Asphalt	Hardened 100 pen Asphalt
$S_{bit,mix}$, $\frac{N}{m^2}$		3.175	11.905

Coree and White (1988) estimated that the mean asphalt penetration in
Indiana was 64. Interpolating for this penetration gives an $S_{bit,visc}$ of
8.572 N/m^2. An assumption is made that the $S_{bit,visc}$ represents and therefore
scales rutting damage. To determine an equivalent amount of traffic using the
ATS when compared to 35 million ESAL, ten year traffic in Indiana; the
$S_{bit,visc}$ corresponding to 35 million ESALs is entered into the equation.
Time of loading equal to 5 mph and a viscosity at a specific temperature is
also entered into the equation. As a result, the number of axle loads (N) can
be determined that would create the same rutting damage $(S_{bit,mix})$ developed
by 10 years of traffic.

Estimates can be made of the number of cycles of loading with the ATS
using the above concept. Initial rutting tests planned with the ATS involve
placement of a three inch bituminous surface on a base concrete slab. Con-
duits in the concrete slab will provide heating to hold the bituminous surfac-
ing temperature constant. With a constant temperature only the bitumen
viscosity at different temperatures needs to be determined. The following
relation is used to estimate the recovered bitumen penetration (ASTM D5) at
20° C.

$$\text{Pen}_r = 0.65 \text{ Pen}_i$$

Using this relation with a Pen_i of 64 results in a Pen_r of 41.6. Two factors might affect the penetration of ATS test sections. First, the duration of any test is expected to be a few days to a few months. Second, a higher rate of hardening might be expected as a result of elevating the test section temperature. Because these factors might be off setting the above relation is considered to be reasonable. A similar assumption for viscosity would be that the viscosity would double. The resulting penetration and viscosity data for an AC-20 asphalt are plotting on Figure 1. Estimates of the number of cycles of loading for the equivalent rutting damage ($S_{bit,visc}$) are given for different temperatures:

Temperature C (F^o)	n poise	N	Days of Operation
38 (100)	10,500	41,853	7.3
60 (140)	4,000	15,944	2.8
82.2 (180)	850	3,388	0.6

In these estimates a loading time of 0.086 sec was used. It is interesting that the decrease from highway speed to the ATS 5 mph testing speed decreases the number of loading cycles by a factor of ten.

These estimates are considered to be approximate but do indicate that rutting damage can be developed with the ATS in a reasonable period of time. Load and tire pressure are two other factors that could be varied and factored into the ATS tests to accentuate rutting damage.

Design of Accelerated Testing Systems

The primary function of the ATS is to apply up to a 20,000 pound load on
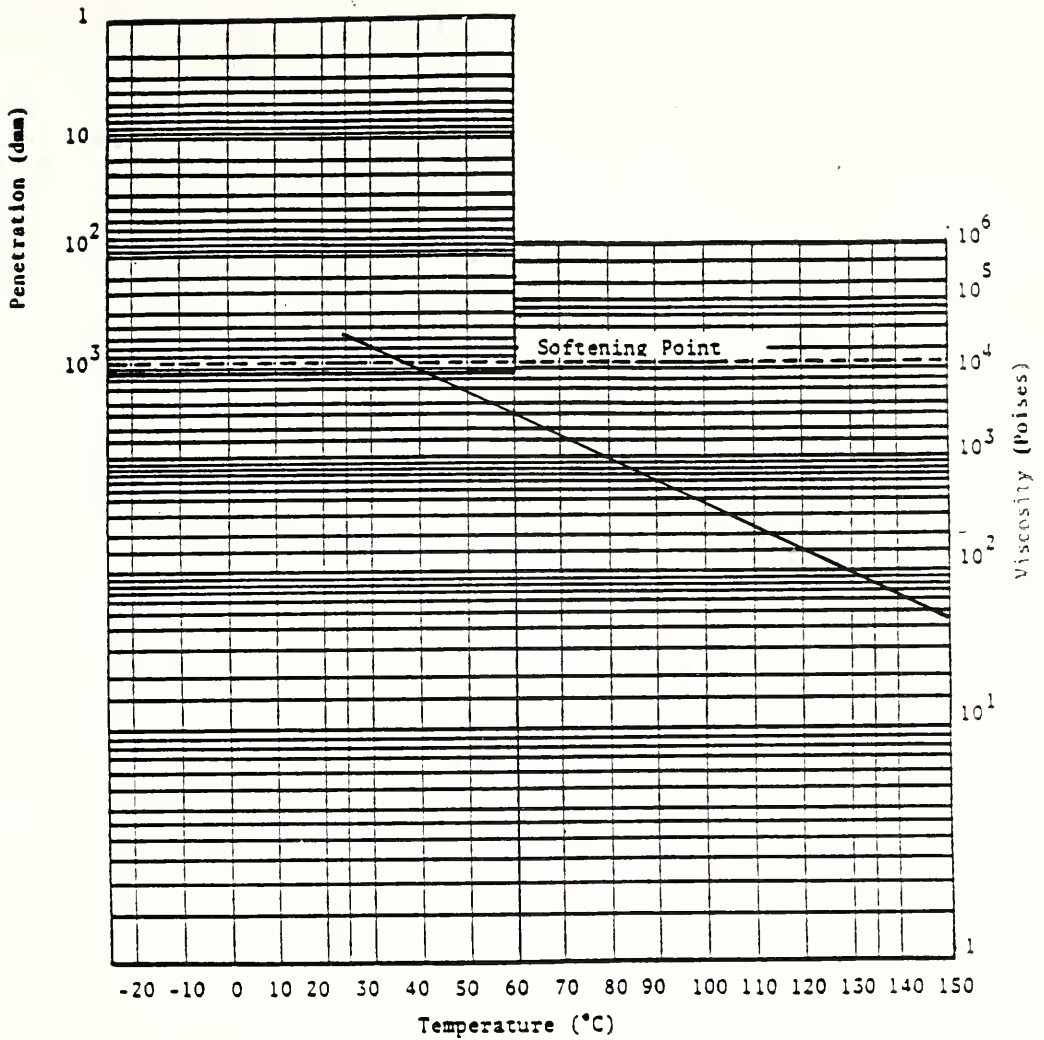
Figure 1.. Bitumen Test Data Chart.

a wheel assembly as it moves across a section of test pavement. The proposed system is unique in that it uses mechanical linkages and springs to provide the loading force. Such a system is much lighter than a system a 20,000 pound mass to generate the load. Since the loading device must move with the wheel assembly, a lighter assembly means the energy required to operate the system will be reduced. This is a major consideration because it will be run continuously. Use of a hydraulic system was considered, but maintenance and the possibility of contaminating the test pavement with hydraulic fluid could not be eliminated easily. A closed loop hydraulic would be expensive.

Reaction forces generated by the loading system are transmitted to the foundation using the structure shown in Figure 2. Figure 2 is a conceptual drawing of the ATS system. A pair of S18 x 54.7 beams run horizontally across the test pit with support structures at each end. The support structures are on rollers so the system can be moved to different lanes of the test pavement. Clamps are used at each end of the structure so that the reaction force of the wheel assembly does not lift the rollers off their tracks. Rollers with a capacity of 10,000 pounds each have been selected to support these loads. The largest stress occurs in the horizontal beams when the wheel assembly is centered between the end supports. Normal stress from bending was calculated for the case of a point load at the middle of a beam which is simply supported at each end. Using a load of 10,000 lb/beam, the stress (σ) was found to be 17.5 ksi, which is well below the 36 ksi yield strength of structural steel (Beer and Johnston, 1981).
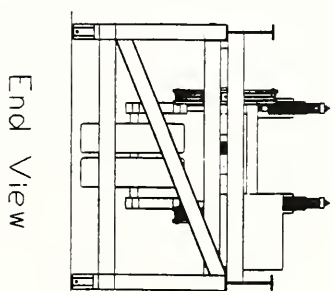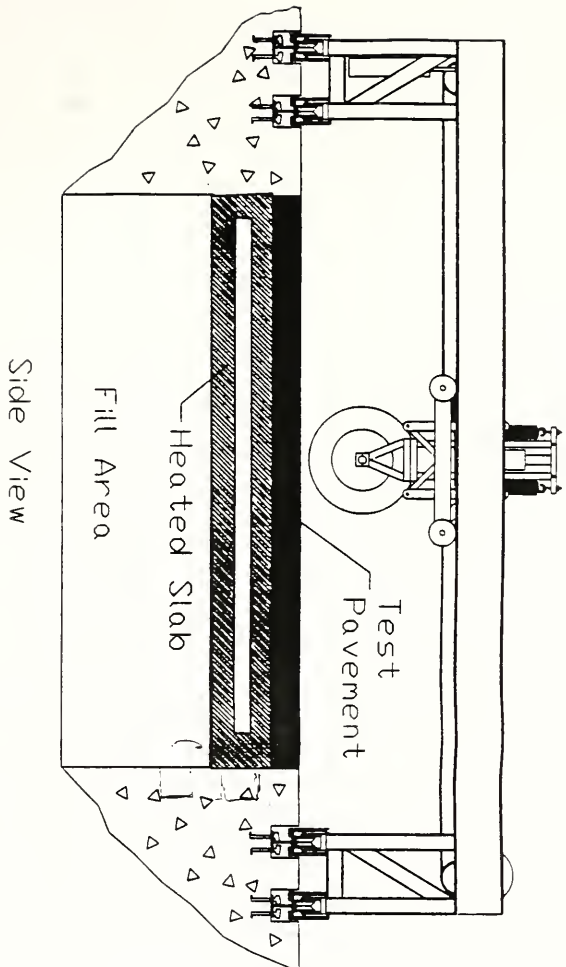
$$\sigma = \frac{Mc}{I}$$

Figure 2. Accelerated Pavement Tester.

Side View

Fill Area

Heated Slab

Test
Pavement

End View

where σ = Bending stress

M = Moment

c = distance extreme fiber

I = moment of Inertia

Since the beams will be continuously loaded and unloaded, fatigue must be con-
sidered. The stress will fluctuate between 0 and 17.5 ksi. This loading is
0.3 times the ultimate strength of 58 ksi, and therefore should not cause
fatigue of the material (Beer and Johnston, 1981; Shigley and Mitchell, 1983).
The maximum beam deflection can be calculated as 0.362 inches using:

$$y_{max} = \frac{PL^3}{48EI}$$

where P = Point load

L = Length of beam

E = Modulus of elasticity

I = Section Modulus

This deflection should not cause binding of the loading assembly as it moves
along the beams. Since the end support provides some resistance to bending,
these calculations based on simply supported ends are conservative.

A constant vertical force is required on the wheel assembly as it travels across the test pavement. However, as the pavement deteriorates, surface irregularities will cause vertical deflection of the wheel assembly. Two mechanisms that would maintain a constant force as they are deflected are being considered (Jenuwine and Midha, 1990 and Nathan, 1985). Figure 3 shows a schematic the constant mechanism developed by Jenuwine and Mida (1990). Figure 4 shows how the mechanism can be implemented on the ATS. Identical mechanisms exert a force of 10,000 pounds on each end of the axle.

Before each pass of the wheel across the pavement, the wheel assembly must be lifted and positioned laterally. Lift will be provided by pneumatic cylinders acting on the constant force mechanism. The power required to complete the lift in 0.25 seconds is 73.5 hp using:

$$\text{Power} = \frac{Fd}{t}$$

where   F = Force

d = distance

t = time

Since lifting is not done continuously, a 5 hp compressor operating during a 6.5 second overall cycle time will be capable of storing sufficient energy in an air tank for the left function. Counteracting the 20,000 pound force directly would require two 10 inch diameter cylinders operating at 125 psi. Use of a mechanical advantage to reduce cylinder diameter is being considered.
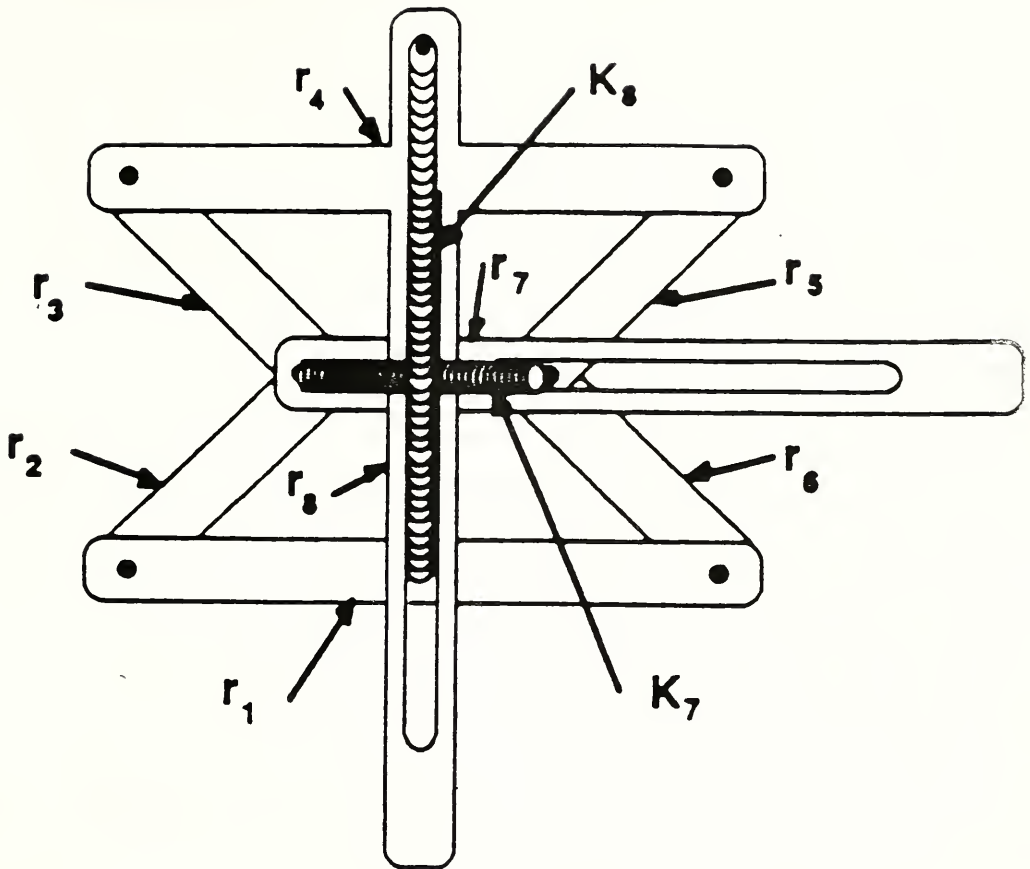
Figure 3. Constant Force Mechanism (Jenumine and Midha, 1990).
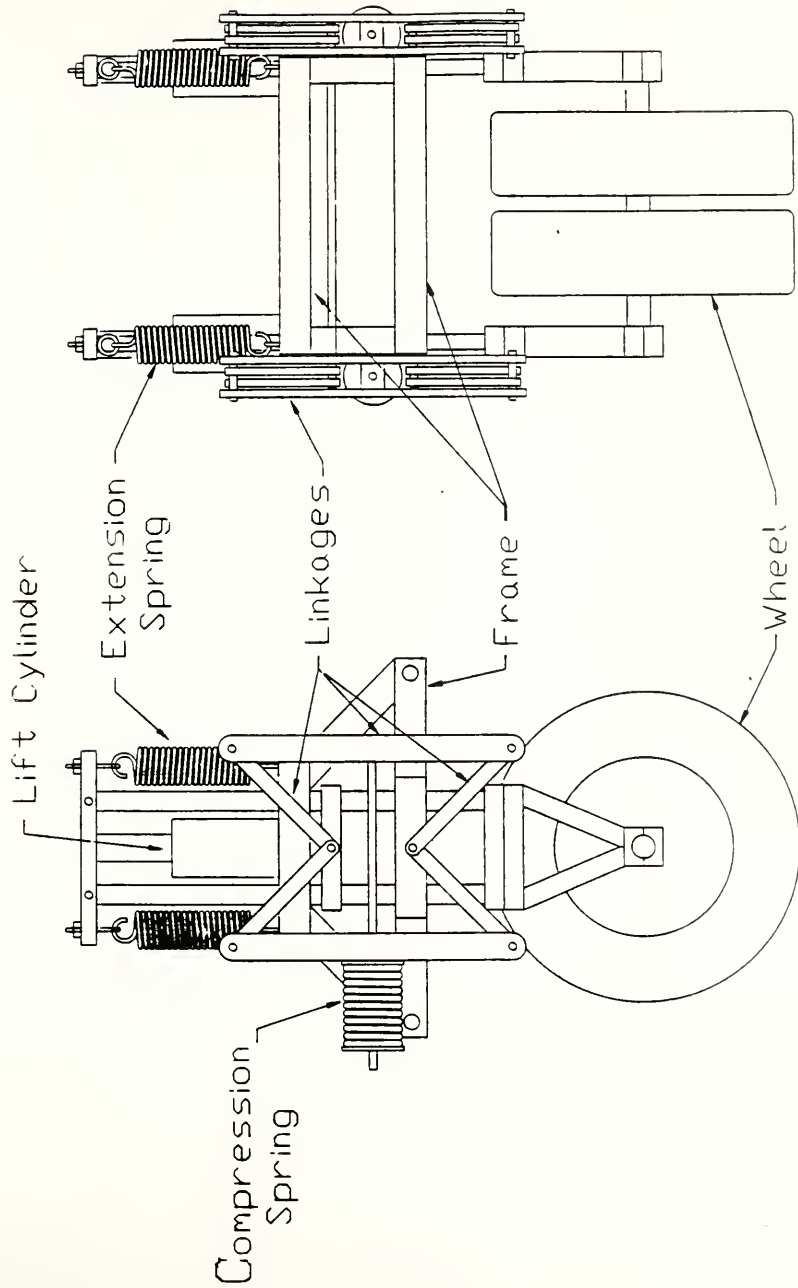
Figure 4. Constant Force Mechanism.

Lateral positioning between cycles is necessary to simulate vehicle wander. This will be provided by an electric motor driving a pair of ball screws, as shown in Figure 5. The highest power requirement will occur when moving 2000 pounds (weight of the wheel assembly) a distance of 12 inches in one second. A two hp motor will be sufficient to provide this capability. The lateral drive system will be located on the moving portion of the ATS, so that its wiring can not be fixed. Power will be supplied through a cord reel suspended from the ceiling of the test facility.

Longitudinal motion of the wheel assembly along the test lane will be provided by a cable drive system which is powered by a 30 hp, 480 volt, 3 phase electric motor. A schematic of this system is shown in Figure 6. The motor will be placed on one of the structure end supports along with the gear box which connects the motor to the cable drum.

Sizing of the main drive system motor was based on rolling resistance of the tires on pavement, rolling resistance of the steel rollers on their rails, and the acceleration required of the wheel assembly at the start of a pass. Tire rolling resistance was calculated to be 240 pounds using:

$$R = fN$$

where   R = Rolling Resistance

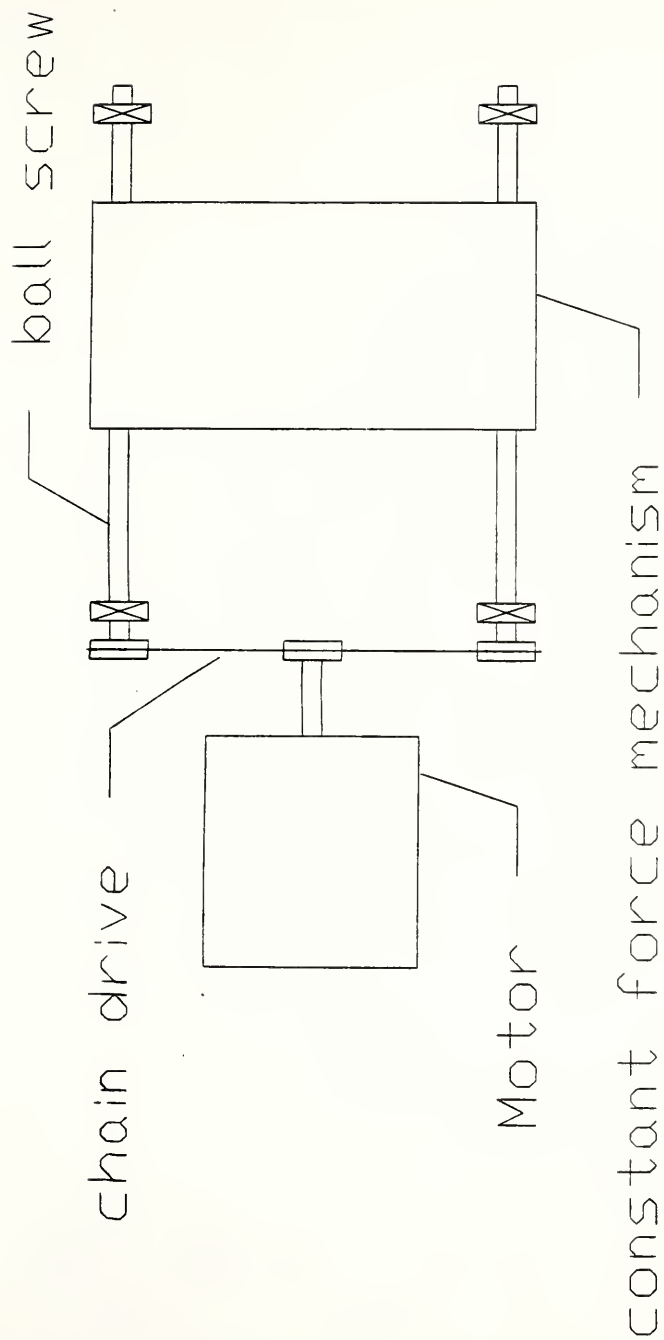f = Rolling resistance coefficient

N = Normal force

Figure 5. Lateral Positioning System.

sheave

cable

carriage

spool

coupling

speed reducer

tensioning weight
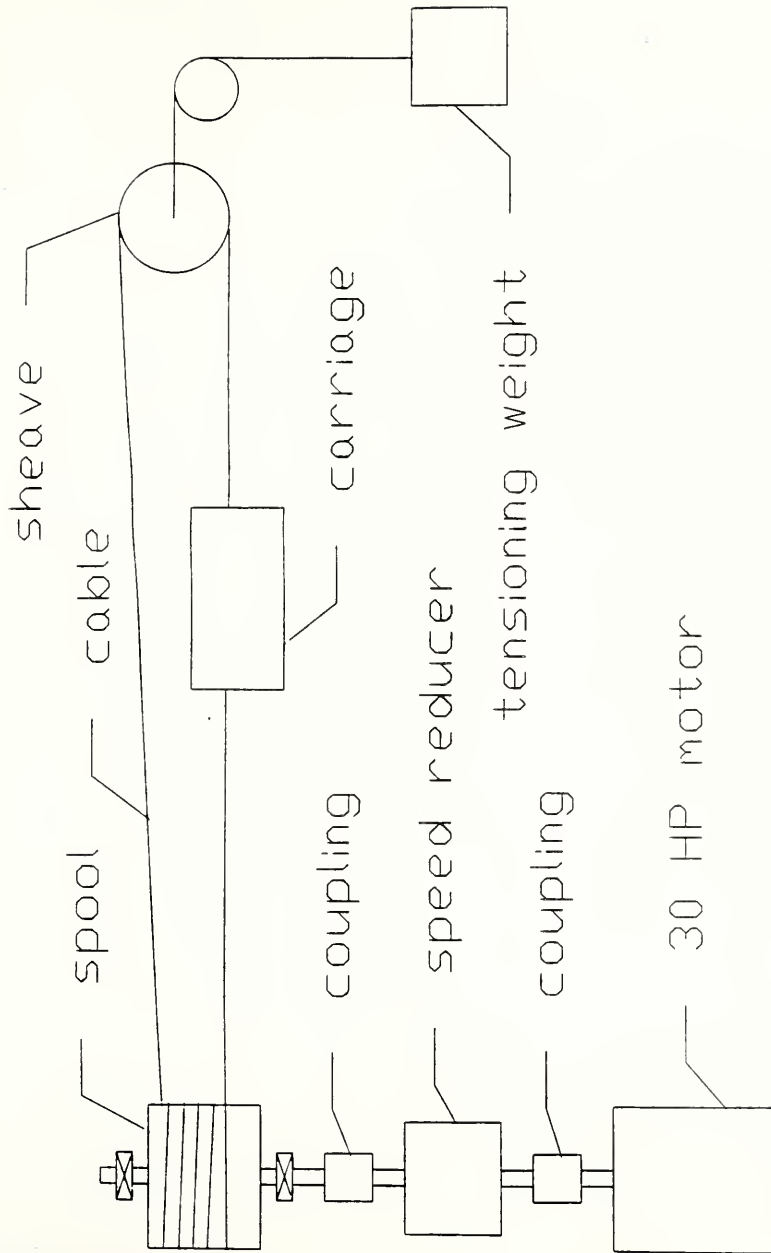
coupling

30 HP motor

Figure 6. Transverse Drive System.

with 0.012 for the coefficient of rolling resistance (Wong, 1978). Rolling

resistance of the steel rollers was calculated to be 200 pounds using a rol-

ling resistance coefficient of 0.01 (Marks Standard Handbook for Mechanical

Engineers, 1978). It is desired to accelerate the 3000 pound assembly to 5

mph in a distance of two feet. Assuming constant acceleration, a value of

13.4 ft/sec/sec is calculated using:

$$a = \frac{v^2}{2s}$$

where   a = acceleration

v = velocity

s = distance

The required force (F) is 1700 pounds using:

$$F = ma + R$$

where   m = mass

a = acceleration

R = Rolling resistance

A conservative estimate of the power requirement can be found by multiplying

this force by the steady state speed of 5 mph. The result is approximately 23

hp. Assuming 75 percent efficiency for the cable drive and gearbox, the power

required at the motor is 30 hp.

A counter weight will be used to maintain tension in the drive cable. This counterweight must provide a force twice the maximum force required to accelerate the wheel assembly. The counterweight must therefore weigh 3400 pounds unless a mechanical advantage is used.

The entire operation of the ATS, as well as all data acquisition, will be controlled by a micro-computer. Two sixteen bit data acquisition boards will be used to interface with the motor controllers and all required sensors. Variable frequency controllers with reversing and soft start options will be used for both the main and lateral drive systems. Position of the system will be monitored with encoders. Limit switches will be used to shut down the system if the wheel assembly should exceed its normal operating zone, and a brake will be engaged if the motor controller cannot stop the assembly because of power failure. The above precautions should be sufficient to prevent a crash of the system.

The purpose of this design synopsis is to demonstrate that the ATS can be built using existing technology. An over all summary and itemized costs are given in Appendix A.

Experimental Design Planning

First application of the ATS will be to study the minimum percent crushed aggregate requirements for bituminous mixtures. Meetings and discussions within INDOT and with industry resulted in the following factors and levels being identified as significant to determining the effect of crushed aggregate on rutting potential of bituminous mixtures.

Factors	Levels
Maximum Aggregate Size (inch)	1/2, 1, 1 1/2
Coarse Crushed Aggregate (%)	40, 70, 95
Bitumen Content (%)	-0.5, Opt. +0.5
Aggregate type	Gravel, Limestone, Slag
Uncrushed sand (% sand fraction)	0, 50, 100

In addition, it is recognized that mix design is a significant factor and would have to be addressed at a number of levels. The ATS will allow additional studies under controlled conditions which will produce data that can be added to a continuing data base on mix performance.

For purposes of simplicity and establishing a starting point the decision has been made to use one maximum aggregate size (one inch) and one surface thickness (three inches). As a result a full factorial of the experimental design would be a 3^4 with 81 total sections. A one-third partial factorial would consist of 27 sections. Only one mix design would be included in this design. The cell structure of this design is shown in Figure 7.

Operational testing of the ATS will be done with a standard bituminous mixture produced by a local plant. Subsequently, the first test sections will be the cells identified X^* and will consist of essentially 100 percent crushed gravel satisfying INDOT specifications for a one inch maximum aggregate size bituminous mixture. As planned, at least three test sections can be installed at the same time for consecutive testing with the ATS. Since the bituminous mixture will be plant produced the logical process would be to calibrate the plant for one aggregate combination and gradation and then vary the bitumen

AGGREGATE TYPE	UNCRUSHED SAND (% SAND FRACTION)	CRUSHED AGGREGATE (%) 40			70			95		
	ASPHALT CONTENT (%)	-.5	Opt	+.5	-.5	Opt	+.5	-.5	Opt	+.5
GRAVEL	0							X*	X*	X*
	50	X	X	X						
	100				X	X	X			
LIME-STONE	0	X	X	X						
	50				X	X	X			
	100							X	X	X
SLAG	0				X	X	X			
	50	X	X	X						
	100							X	X	X

Figure 7.   Preliminary Experimental Design.

content. The result of this approach to producing the mixtures is to limit the statistical analysis to a study of the first order effects except for asphalt content.

The aggregate industry has supported the planning process and has solicited aggregate producer participation to supply aggregate for the study. A local contractor has indicated a willingness to cooperate in producing and placing the bituminous mixtures. Information is being acquired on consistency of asphalt supplies so that the same asphalt can be used for all test sections.

Summary

The major questions associated with Phase I of the HPR Part II project, "Determining Percent Crushed Aggregate Requirements in Bituminous Mixtures" have been answered. Operating characteristics of the ATS have been determined that would produce the accelerated structural and rutting damage. Estimates have also been made of the time to produce these distresses. In both cases the time is well within the one year criteria initial adopted.

A more detailed design of the ATS has been completed and costs have been estimated that appear to be close to the original estimate. Even with commercial labor rates the costs are well below costs suggested by early review comments.

Significant planning has been accomplished on the experimental design. This process ahs benefited from cooperative participation by INDOT and Purdue University staff as well as the aggregate industry. Broader interests have been indicated thru contractor participation.

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Appendix A: Estimated Costs of Accelerated Testing System

The following cost estimate is based on a preliminary design of the accelerated testing system (ATS). Wherever possible, prices for stock components were taken from catalogs. Parts which must be fabricated have been developed far enough to estimate the amount of material required and the number of man-hours required for construction. Material costs were estimated at 60 cents per pound of steel required. Commercial labor costs have been estimated at $40 per man-hour. However, alternate labor costs are also discussed. Total cost of the ATS is estimated to be $107,888.

A breakdown by major subsystem is as follows:

Support Structure .	$41,323
Main Drive System	15,769
Lateral Positioning System	1,910
Wheel Assembly	4,891
Constant Force Mechanism	14,496
Constant Force Mechanism Carriage	1,499
Controls and Data Acquisition	20,000
Assembly Labor (160 man hours)	8,000

$107,888 Total

On a proportional basis the materials costs and commercial rate labor costs are:

Total Cost	$107,888
Material Costs	36,000
Commercial Labor Costs	72,000

As noted above, the commercial hourly rate is $40 per hour. Two alternative hourly rates are available within the University Shops. The Central Machine Shop hourly rate is $25 per hour and the Mechanical Engineering Machine Shop hourly rate is $20 per hour. If a 50 percent split of the work is taken between the Central Machine Shop and Mechanical Engineering Machine Shop the effective hourly rate would be $22.50 per hour. As a result the labor costs for the ATS would be reduced to $40,500 or a total cost of $76,500. There are one or two other savings that could be realized but will not be applied at this time.